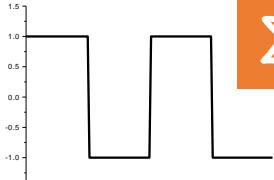
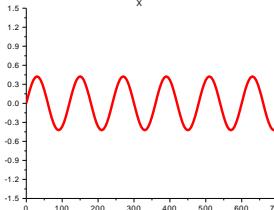


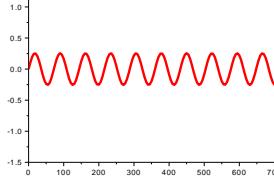
Σύνθεση Fourier



$$4/\pi \quad \sin \omega_0 \chi$$



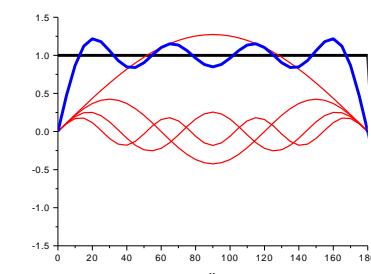
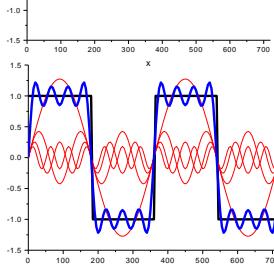
$$4/3\pi \quad \sin 3\omega_0 \chi$$



$$4/5\pi \quad \sin 5\omega_0 \chi$$



$$4/7\pi \quad \sin 7\omega_0 \chi$$

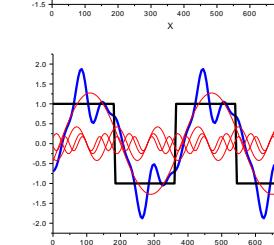
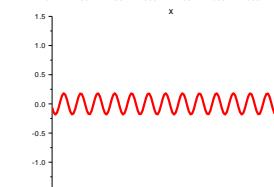
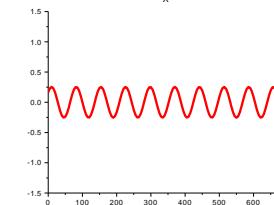
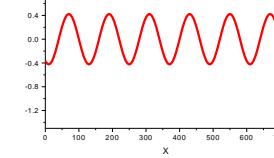
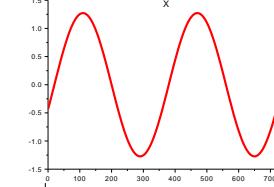
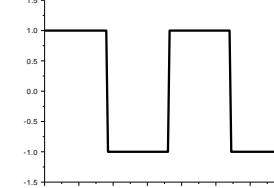
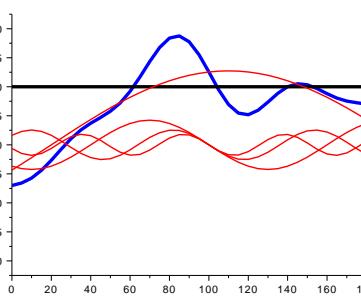


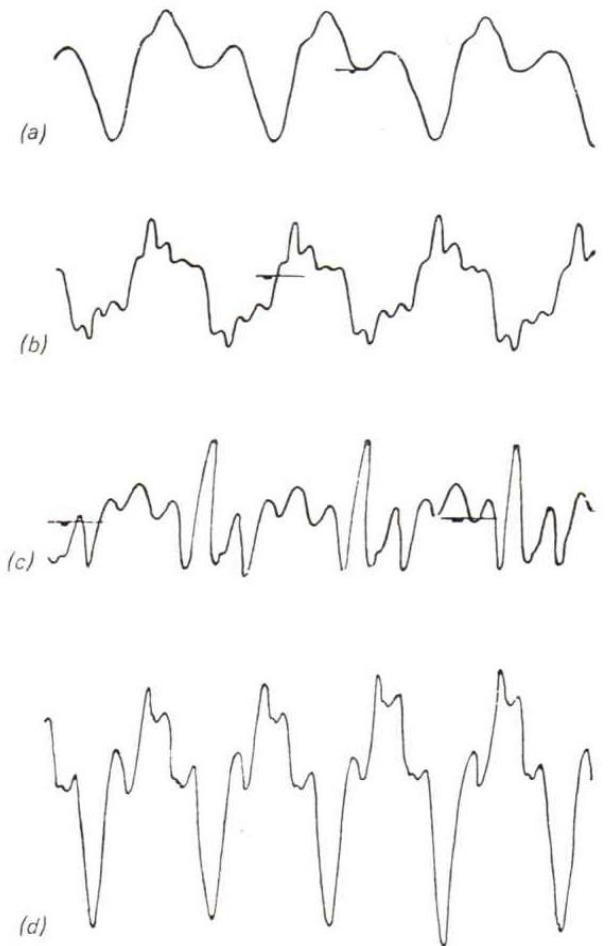
$$4/\pi \quad \sin \omega_0 \chi$$

$$4/3\pi \quad \sin 3\omega_0 \chi$$

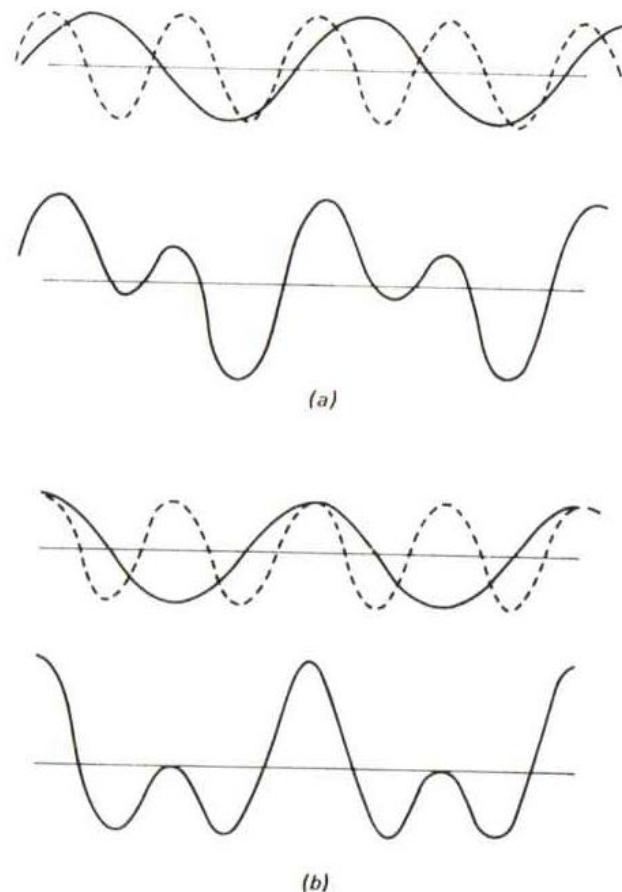
$$4/5\pi \quad \sin 5\omega_0 \chi$$

$$4/7\pi \quad \sin 7\omega_0 \chi$$





3. 1. The variation in the pressure of the air for a note from (a) flute
(b) clarinet, (c) oboe, (d) saxophone.

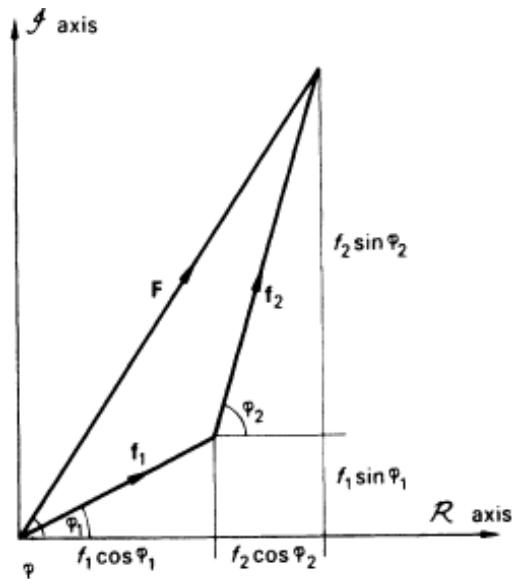


$$\rho(\mathbf{x}) = \frac{1}{V} \sum_{\mathbf{h}} \mathbf{F}(\mathbf{h}) \exp(-2\pi i \mathbf{h} \cdot \mathbf{x})$$

$$\rho(XYZ) = \frac{1}{V_c} \sum_{\text{all } h,k,l} |F| \cos [2\pi(hX + kY + lZ) - \alpha].$$

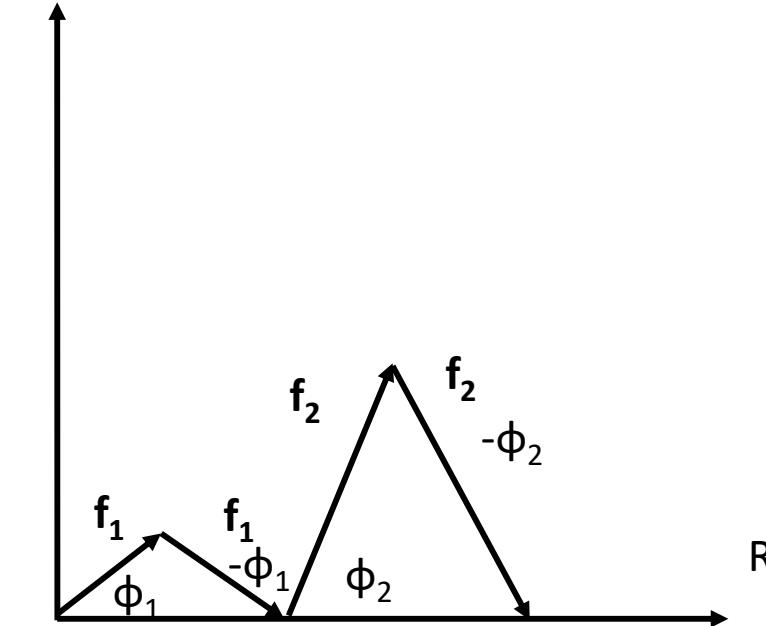
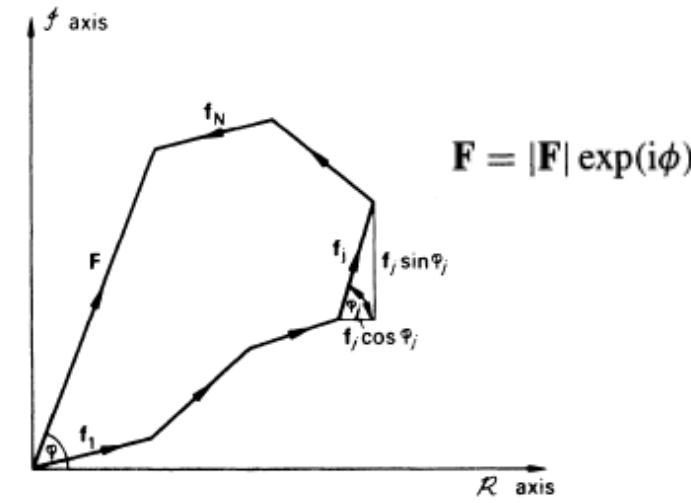
$$F(\vec{H}) = F_{(h,k,l)} = \sum_{j=1}^N f_j \cdot e^{2\pi i \vec{H} \cdot \vec{r}_j}$$

$$\mathbf{F} = f_1 \exp(i\phi_1) + f_2 \exp(i\phi_2) + \cdots + f_j \exp(i\phi_j) + \cdots = \sum_{j=1}^n f_j \exp(i\phi_j)$$



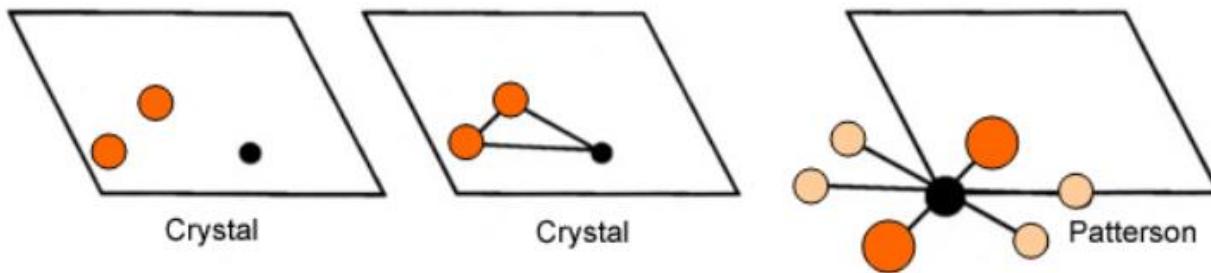
$$\bar{r}_j \quad -\bar{r}_j$$

$$F(\vec{H}) = \sum_{j=1}^{N/2} (f_j e^{2\pi i \vec{H} \cdot \bar{r}_j} + f_j e^{-2\pi i \vec{H} \cdot \bar{r}_j}) = \pm |F(\vec{H})|$$



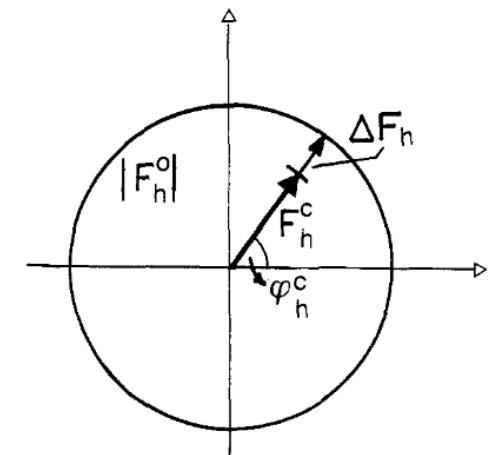
Συνάρτηση Patterson

$$P(u) = \int \rho(x) \cdot \rho(x+u) du = \frac{1}{V} \sum_h |F_{obs}(h)|^2 \cdot e^{-2\pi i h \cdot u}$$



Συνθεση Fourier διαφορών

$$\Delta\rho(x, y, z) = \frac{2}{V_c} \sum_h \sum_k \sum_l (|F_o| - |F_c|) \cos[2\pi(hx + ky + lz) - \phi_c]$$



Άμεσες μέθοδοι

Κανονικοποιημένοι παράγοντες δομής

$$\left| E(\vec{h}) \right|^2 = \frac{\left| F_{\text{rel}}(\vec{h}) \right|^2 K(S)}{\varepsilon \sum_{j=1}^N f_j^2}$$

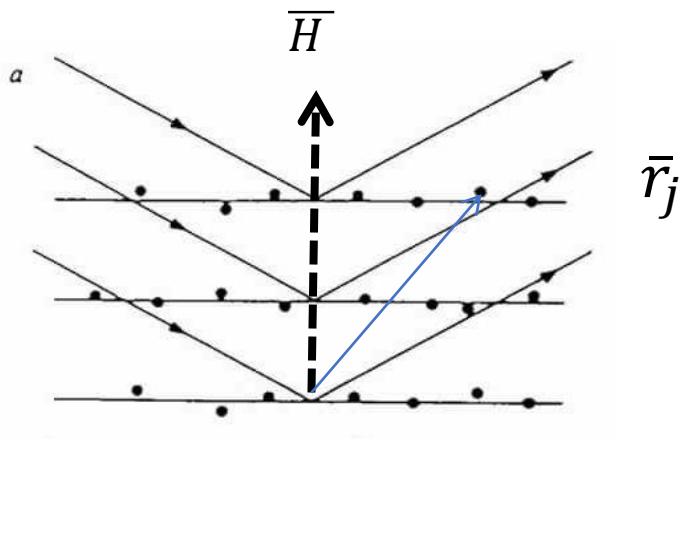
$$S[E(\vec{h}_1)] S[E(\vec{h}_2)] S[E(\vec{h}_3)] \cong +1$$

Κεντροσυμμετρικές δομές

$$\varphi(\vec{h}_1) + \varphi(\vec{h}_2) + \varphi(\vec{h}_3) \cong 0$$

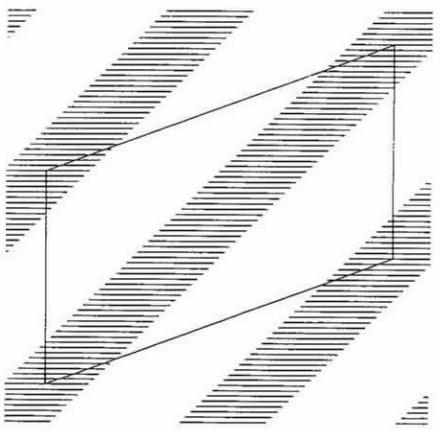
μη Κεντροσυμμετρικές δομές

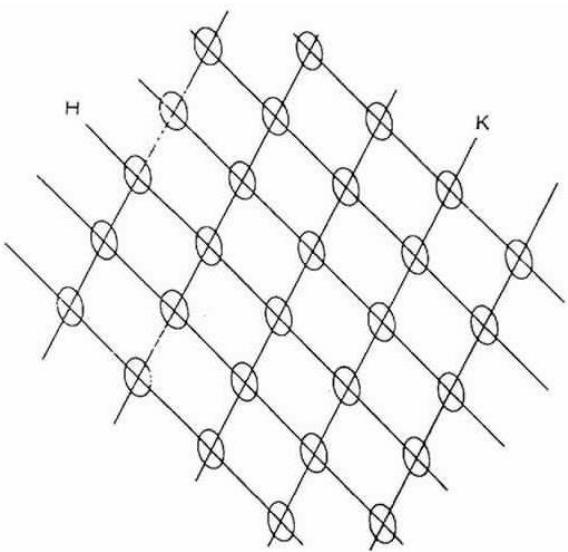
$$\vec{h}_1 + \vec{h}_2 + \vec{h}_3 = 0$$



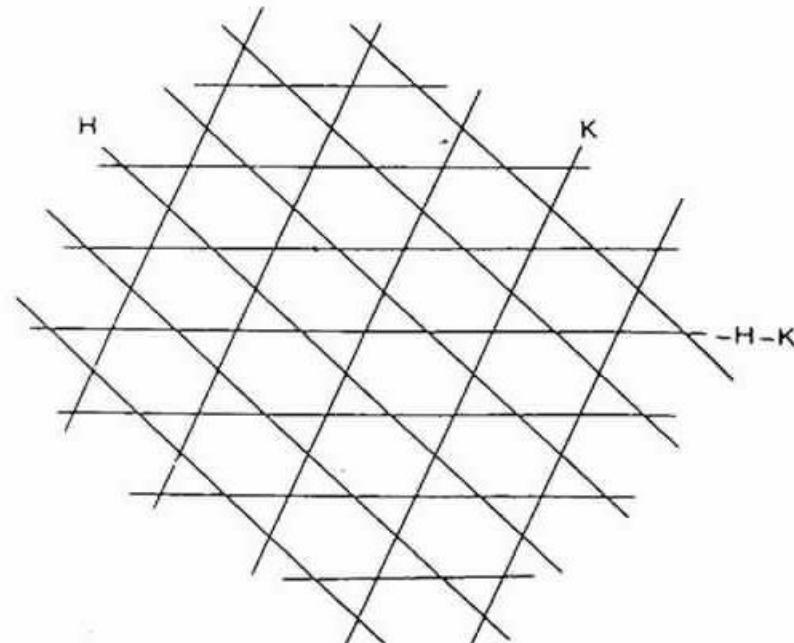
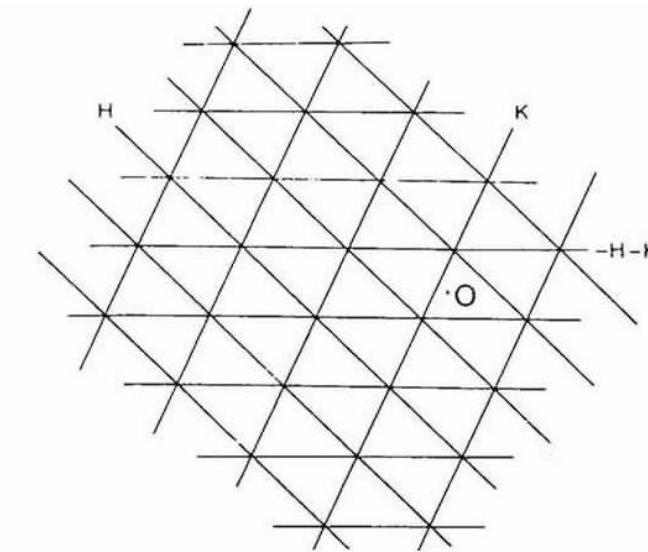
$$F(\vec{H}) = F_{(h,k,l)} = \sum_{j=1}^N f_j \cdot e^{2\pi i \vec{H} \cdot \vec{r}_j} :$$

$$F(\bar{H}) = \sum_{j=1}^N f_j e^{2\pi i (\frac{1}{d})(nd)} \approx \sum_{j=1}^N f_j$$





$$\vec{h}_1 + \vec{h}_2 + \vec{h}_3 = 0$$



$$\varphi_{\bar{H}1} \quad \varphi_{\bar{H}2} \quad \varphi_{\bar{H}3} \quad \bar{H}1 + \bar{H}2 + \bar{H}3 = 0$$

$$\varphi_{\bar{H}4} \quad \varphi_{\bar{H}5} \quad \bar{H}1 + \bar{H}4 + \bar{H}5 = 0$$

$$\begin{matrix} \cdot & \cdot \\ \cdot & \cdot \\ \cdot & \cdot \\ \cdot & \cdot \end{matrix}$$

$$\varphi_{\bar{H}n1} \quad \varphi_{\bar{H}n2} \quad \bar{H}1 + \bar{H}4 + \bar{H}5 = 0$$

<https://www-structmed.cimr.cam.ac.uk/Course/Fourier/Fourier.html>

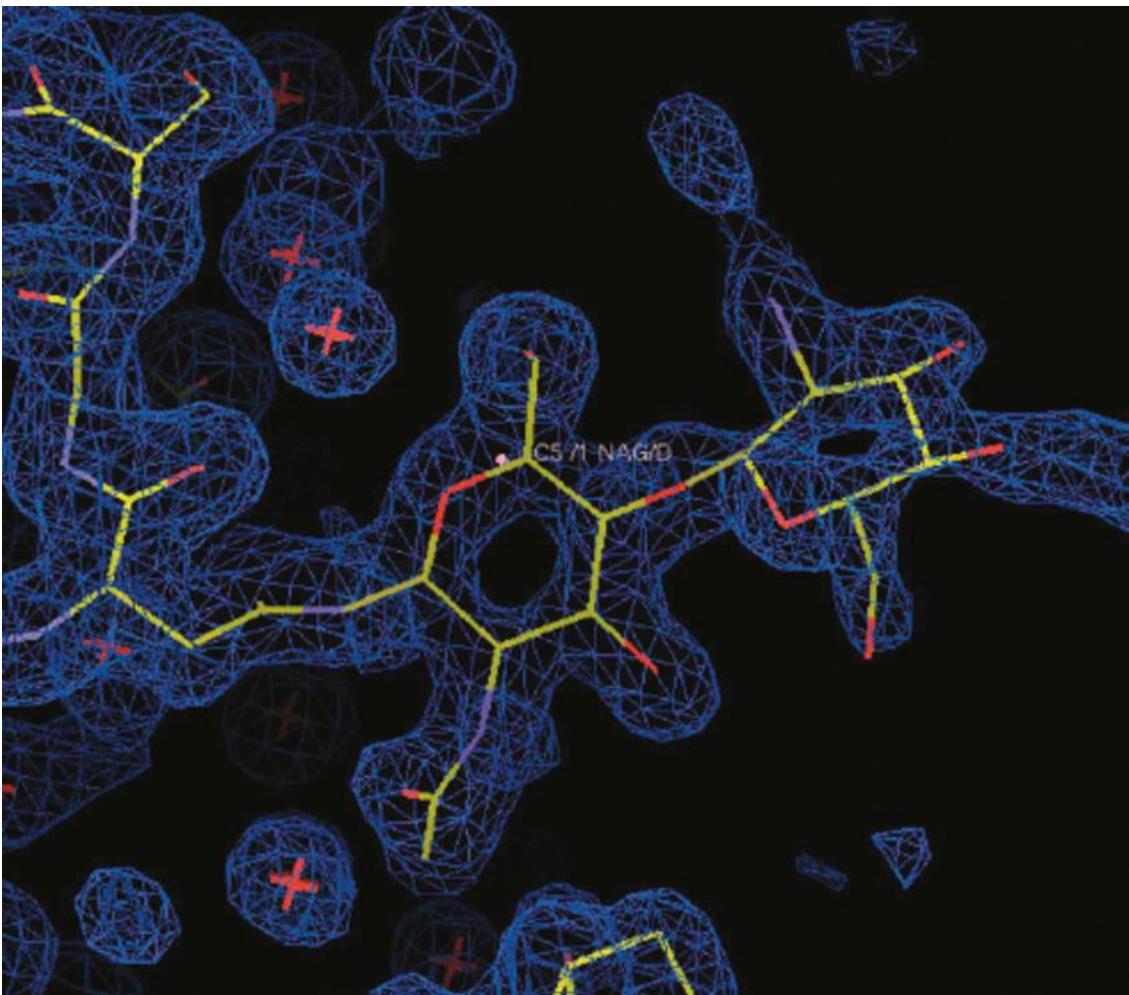
Jerome Karle



Herbert A. Hauptman



Nobel price in Chemistry
1985



$$\rho(XYZ) = \frac{1}{V_c} \sum_{\text{all } h,k,l} |F| \cos [2\pi(hX + kY + lZ) - \alpha].$$

....Linear fit

....non Linear fit

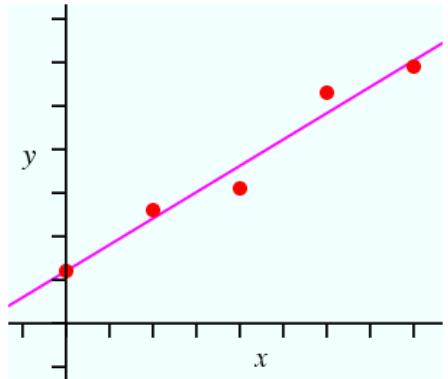


Figure B

$$y = m x + c$$

$$M = \sum w(|F_o| - |F_c|)^2$$

$$f(x + \Delta x) = f(x) + \Delta x \frac{df(x)}{dx} + \frac{(\Delta x)^2}{2!} \frac{d^2 f(x)}{dx^2} + \frac{(\Delta x)^3}{3!} \frac{d^3 f(x)}{dx^3} + \dots$$

[Birkbeck College, University of London.](#)

During the integration of the reflections (peaks), the intensities are determined by $I = I_{\text{reflection}} - I_{\text{background}}$

For weak reflections the result can be negative.

Reflections with $0 > I > -3\sigma(I)$ contain useful information. ($I = 0$ is in the margin of errors for these reflections.)

Merging of Reflections – R(int)

$$R_{\text{int}} = \frac{\sum |F_o^2 - F_o^2(\text{mean})|}{\sum F_o^2}$$

R(int): Merging error (measure of the precision/reproducibility)

Possible error sources (high R(int) value):

- Incorrect Laue group
- Bad or missing absorption correction
- Crystal decomposition
- Twinning
- Goniometer problems (covered reflections, misalignment)

Merging of Reflections – R(sigma)

$$R_{\text{sigma}} = \frac{\sum \sigma(F_o^2)}{\sum F_o^2}$$

R(sigma) - Measure of the signal-to-noise ratio

$$M = \sum w(|F_o| - |F_c|)^2$$

(The lower M, the better is the agreement of our model with the experimental data.)

$$w_{hkl} = 1/[\sigma^2(F_{o,hkl})^2 + (a P)^2 + b P]$$

The values for a and b are chosen to give an even distribution of the variances across all groups of data based on the relative intensities

But: M increases with the number of reflections and with their intensity. It is thus structure dependent, with well diffracting structures with high redundancy giving the highest M values. We thus need a structure independent value.

$$M' = \sum w(|F_o|^2 - |F_c|^2)^2$$

R2 →

Confidence factor, Residual, R-factor:

$$wR_2 = R_w(F^2) = \sqrt{\frac{\sum w(F_o^2 - F_c^2)^2}{\sum w(F_o^2)^2}}$$

For statistical reasons, refinement against F^2 gives R-factors approximately twice as high than those for refinement against F . To facilitate comparison (and to increase acceptance of the new method) SHELXTL calculates also the R-factor based on F .

$$R_1 = \frac{\sum |F_o| - |F_c|}{\sum |F_o|} \quad \leftarrow R1$$

SHELXL calculates 4 confidence values:

- wR2 (all data)
 - wR2 (observed data, $I > 2\sigma(I)$)
 - R1 (all data)
 - R1 (observed data, $I > 2\sigma(I)$)
- Refinement against F^2 requires a correct weighing scheme
The weighing schemes optimised for refinement against F^2 cannot be used for the calculation of R1.

The important values are wR2 (all data) (since we do the refinement with all data) and R1 (observed data), for comparison with the old method.

	Good	Acceptable	Problematic	Really problematic
R1	< 5%	< 7%	>10%	>15%
wR2	< 12%	< 20%	>25% (or $\text{ou} > 2 \cdot \text{R1}$)	>35%
S	0.9-1.2	0.8-1.5	<0.8 or $\text{ou} > 2$	<0.6 or $\text{ou} > 4$

Goodness-of-Fit - S

The GoF or GooF is another value which describes the quality of our model:

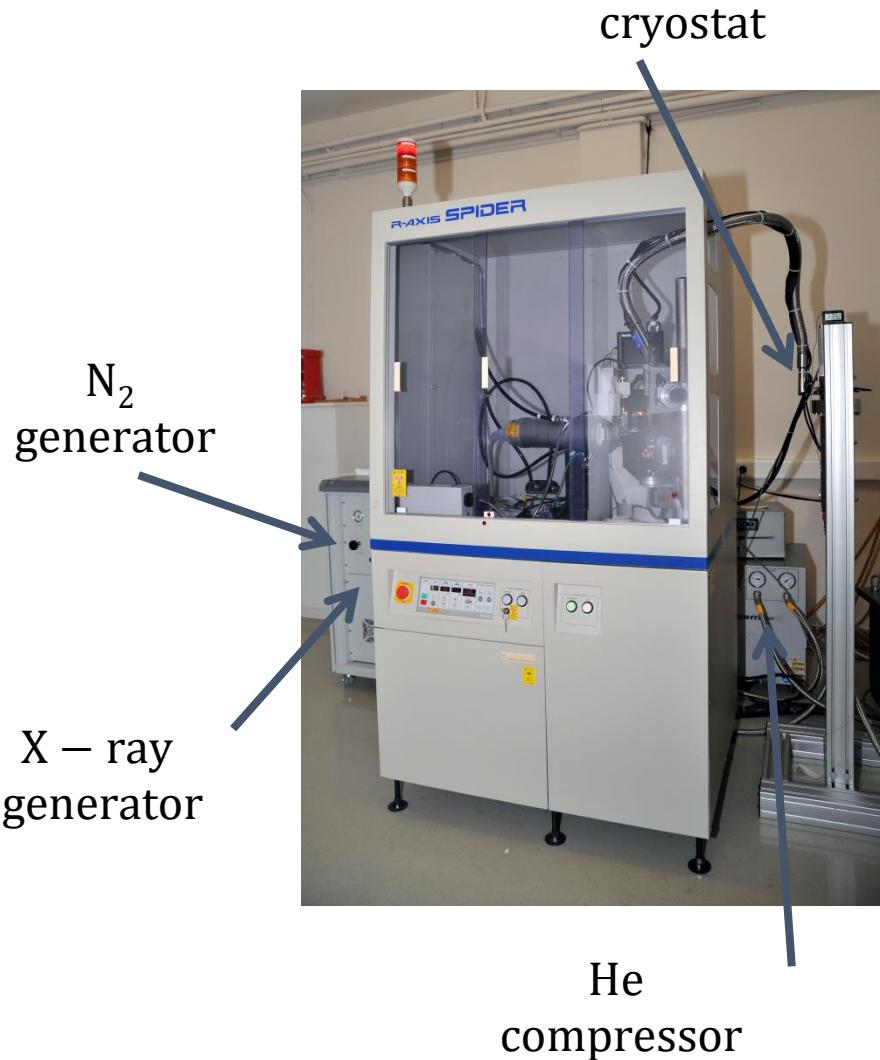
$$GooF = S = \sqrt{\frac{\sum w(F_o^2 - F_c^2)^2}{N_{Ref.} - N_{Par.}}}$$

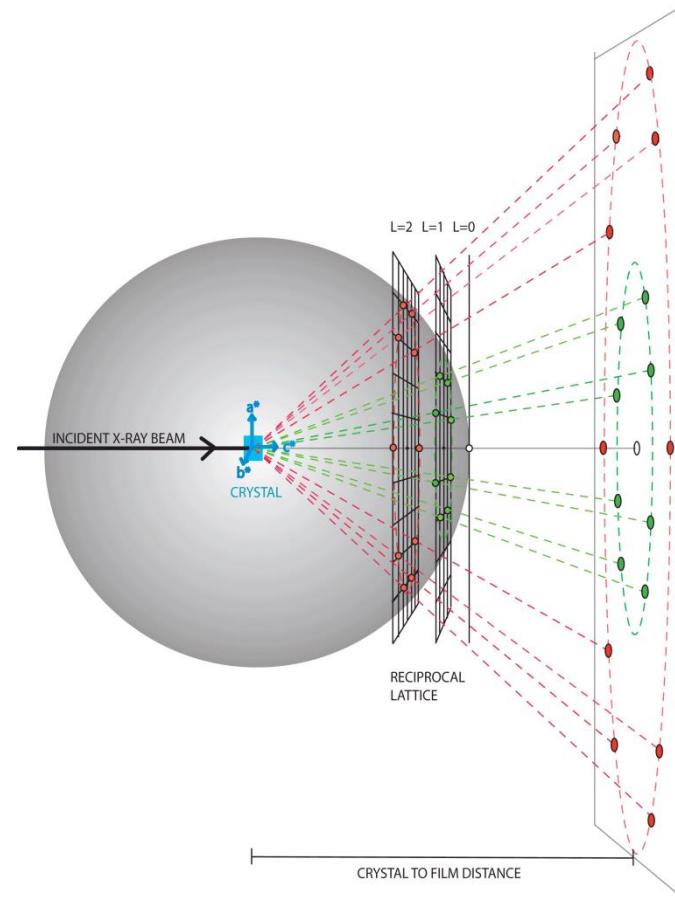
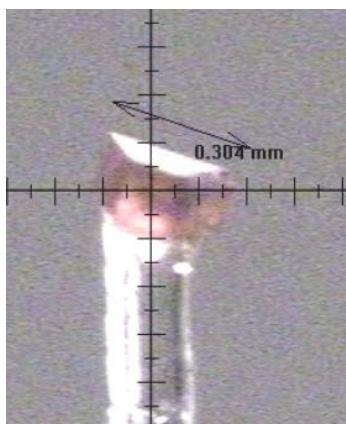
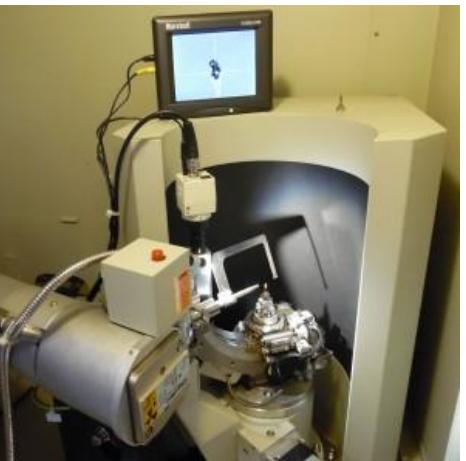
$N_{Ref.}$: number of independent reflections, $N_{Par.}$: number of parameters

S should be around 1 for a good structure

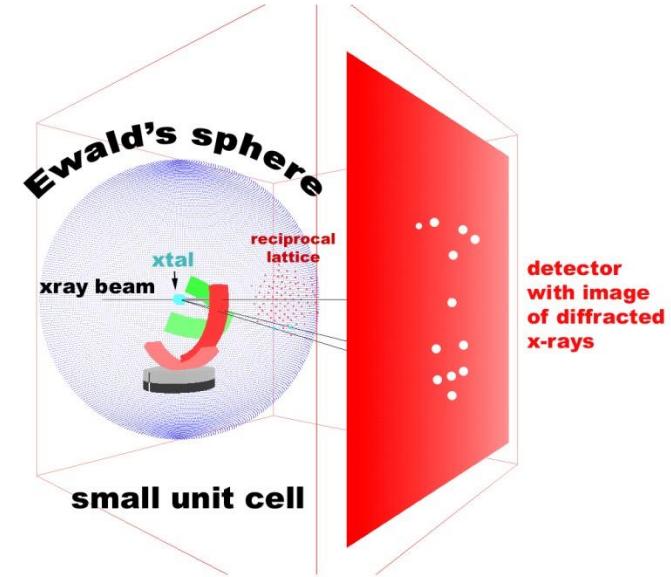
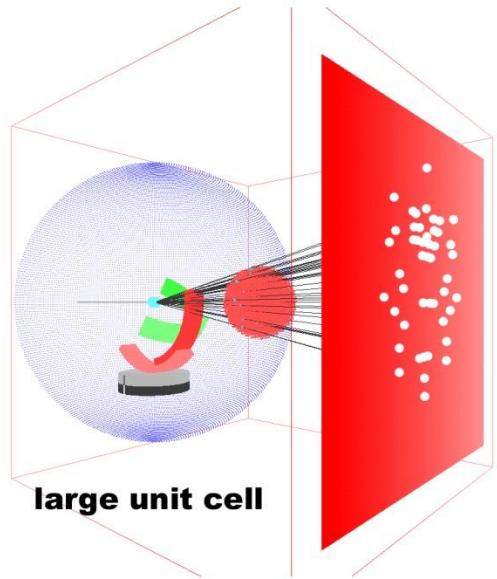
S > 1: bad model or bad data/parameter ratio

S < 1: model is better than the data - problems with the absorption correction, outlier reflections at low resolution





OSCILLATION ANGLE



**fewer degrees
oscillation**

- + less risk of spot overlap
- requires more exposures, time consuming
- + more accurate intensity measurements

**more degrees
oscillation**

- more risk of spot overlap -
- requires fewer exposures, quicker collection +
- less accurate measurements -

